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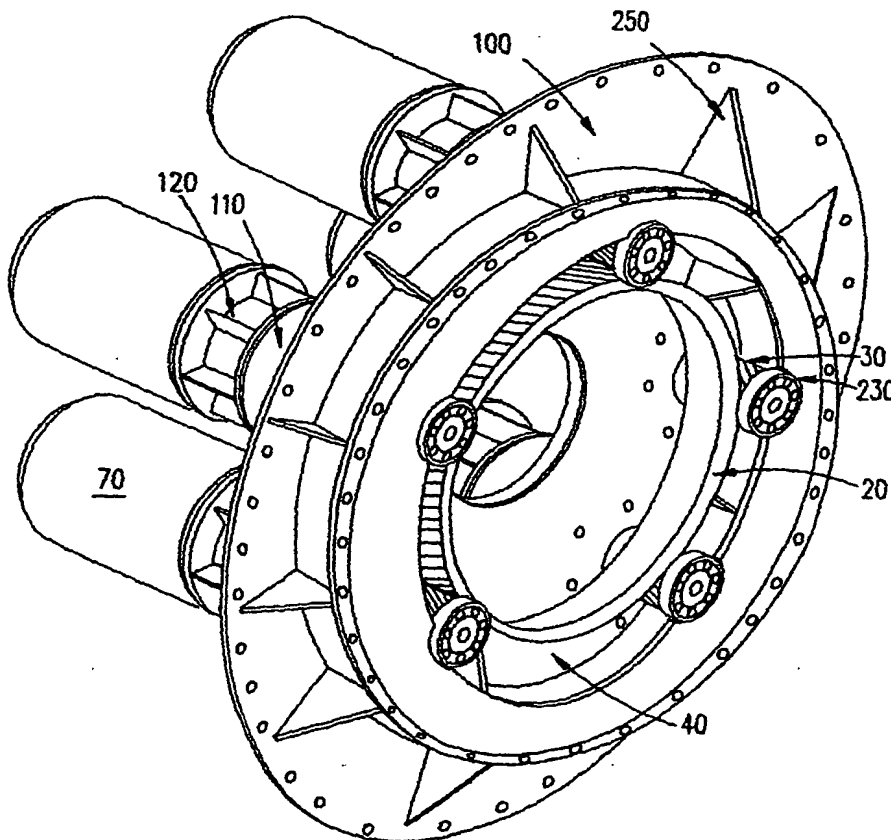
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- (71) Applicant (for all designated States except US):
DEHLSSEN ASSOCIATES, L.L.C. [US/US]; 714
Bond Avenue, Santa Barbara, CA 93103 (US).
- (72) Inventors; and
(75) Inventors/Applicants (for US only): DEHLSSEN, James, G., P. [US/US]; 200 San Ysidro Road, Montecito, CA 93108 (US). DEANE, Geoffrey, F. [US/US]; 5080 San Simeon Drive, Santa Barbara, CA 93111 (US).
- (74) Agents: PALMER, John et al.; Ladas & Parry, 5670 Wilshire Boulevard, Suite 2100, Los Angeles, CA 90036-5679 (US).

[Continued on next page]

(54) Title: POWERTRAIN FOR POWER GENERATOR



(57) Abstract: Powertrains for high torque, low RPM wind turbines and ocean current turbines. The turbine consists of a large, input power shaft-mounted, rotating sun-gear with stationary powertrains mounted around its periphery. The gear teeth on the sun gear rotate past the teeth on the pinions, causing the pinions to turn and delivering power to each smaller powertrain. Alternatively, the powertrains are attached in a spindle around the perimeter of a main power input drive shaft, and rotate as the shaft rotates. Each input drive shaft to smaller powertrain gearboxes is fitted with a pinion. As the main power input shaft turns, the generators, gearboxes and pinions rotate, moving the pinions around the interior of a stationary ring gear. Reduction and distribution of torque is similar to the sun-gear embodiment of the powertrain. In the sun-gear configuration, each smaller powertrain is stationary, reducing stress caused by rotation.

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POWERTRAIN FOR POWER GENERATOR

BACKGROUND OF THE INVENTION

Field of the Invention

This invention relates to electric power-generating devices such as wind turbines and ocean current turbines, and more particularly to a method and apparatus for distributing to various gearboxes the input torque characteristic of low rotational velocity high-torque operation of wind or water turbine blades.

BACKGROUND

Many electric power-generating devices, such as wind turbines and ocean current turbines, benefit from economies of scale, yielding lower costs for generated electricity with larger power generation per unit. This increase in power is often accompanied by a reduction in rotational velocity of the power input shaft, resulting in a large increase in torque. Because electric generators require rotational velocities tens to hundreds of times greater than the rotational velocity of the input shaft, a speed increasing gearbox is often applied between the power input shaft and the generator. Generally, torque (τ) delivered by the power input shaft to the speed-increasing gearbox for such applications is given by

$$\tau = P / \omega \quad (1)$$

where P is the power and ω is the rotational velocity of the power input shaft. Costs of conventional gearboxes (planetary, helical, etc.) increase exponentially with increased torque, diminishing the beneficial effects of increased scale. In addition, such high torque gearboxes must generally be custom designed and manufactured for specific application, further increasing their costs.

It is desirable to provide a way of reducing the torque on gearboxes resulting from slow moving turbine blades.

1 Prior art shows several inventions with multiple motors driving a single power
2 output shaft, an application significantly different than the present application. Electric
3 generating systems have been shown in the art to use multiple generators powered by a
4 single gearbox. In each invention, the division of this power generating capacity to the
5 multiple generators is done for power quality considerations. Division of gearboxes is
6 becoming rare in recent commercial applications, largely because the cost of many small
7 generators often exceeds the cost of a single large generator with the same capacity.
8

9 In addition, as turbines grow in size, the size and weight of individual components
10 grow as well. Wind turbines place these components on top of a tower, presently
11 stretching to over 60m above the ground, while ocean current turbines are located at sea,
12 where they can only be accessed by boat. The size of the components necessitates very
13 large lifting equipment, making both the land-based cranes and ocean lifting equipment
14 extremely costly. It is desirable to provide a way of reducing the weight and size of
15 individual components of electricity generating equipment.
16

17 By dividing the powertrain into smaller components, generating systems receive
18 an element of redundancy. For example, when ten small gearboxes and generators split
19 the system's load, if one gearbox or generator experiences a fault, the system's capacity
20 may only be reduced by 10%, allowing the system to remain active. A single set of
21 components loses all of its capacity when a single component experiences a fault. It is
22 desirable to provide a way of establishing reliability through redundancy in generating
23 systems.
24

25 SUMMARY OF THE INVENTION

26 Briefly, in accordance with the invention, an electric power-generating device
27 comprises a rotor which revolves in response to an external source of mechanical energy
28 to which is coupled a main power input shaft. A torque-dividing gearbox is coupled to the
29 main power input shaft and a plurality of torque-reducing gearboxes, each driving a
30 generator and each having an input shaft, are connected to the torque-dividing gearbox.
31 The plurality of torque-reducing gearboxes are located around a perimeter of the main
32 power input drive shaft.

1 In accordance with an embodiment of the present invention, a powertrain for wind
2 turbines and ocean current turbines consists of a large, input power shaft-mounted,
3 rotating sun-gear with stationary smaller powertrains mounted around its periphery. The
4 gear teeth on the sun gear rotate past the teeth on the pinions, causing the pinions to turn
5 and deliver power to each smaller powertrain. Alternatively, powertrains are attached in a
6 spindle around the perimeter of a main power input drive shaft, and rotate as the shaft
7 rotates. The input drive shaft to each of the smaller powertrain gearboxes is fitted with a
8 pinion. As the main power input shaft turns, the generators, gearboxes and pinions rotate,
9 moving the pinions around the interior of a stationary ring gear. Reduction and
10 distribution of torque is similar to the rotating sun-gear powertrain. In the sun-gear
11 configuration, each smaller powertrain is stationary, reducing stress caused by rotation.
12

13 BRIEF DESCRIPTION OF THE DRAWINGS

14 The invention will be described in detail with reference to the drawings in which:

15 **FIGURE 1** illustrates a cut-away side view of the preferred embodiment of the
16 distributed powertrain.;

17 **FIGURE 2** shows an enlarged view of the components of the present invention;

18 **FIGURE 3**, is a perspective view of a first embodiment of the invention showing
19 a distributed powertrain having five units mounted inside of a nacelle; and,

20 **FIGURE 4** is a cutaway view of a second embodiment of the invention showing a
21 distributed powertrain having units mounted inside of a nacelle.

22 **FIGURE 5** is a schematic diagram illustrating prior art.

23 **FIGURE 6** is a schematic diagram of the present invention.
24

25 DESCRIPTION OF THE PREFERRED EMBODIMENTS

26 **FIGURE 1** is a cut-away view of the preferred embodiment of the distributed
27 powertrain. Power, supplied by the flow-driven rotation of the rotors, is transmitted into
28 the nacelle by the rotating main shaft 10. A torque-dividing gearbox, comprising a sun
29 gear 20, pressure-mounted on the perimeter of the main shaft and rotating with the shaft,
30 interacts with five pinions 30 mounted around its perimeter, causing them to turn at a
31 rotational rate greater than that of the sun-gear. The chamber 40 in which the sun-gear
32 and pinions rotate is flooded with oil or contains an oil distribution system for

1 lubrication. Each pinion is coupled to the input end of a small torque-reducing gearbox,
2 which increases the rotational speed of the output shaft relative to the pinion. The output
3 shaft of each gearbox is connected by a coupling 60 to a generator 70. Each sub-
4 powertrain consisting of a gearbox 50 and generator 70 is mounted to a circular plate 100
5 comprising one wall of the oil-filled pinion chamber 40. Each gearbox 50 is held within a
6 plate-mounted gearbox flange 110, to which is mounted a generator flange 120. The
7 generator 70 is then mounted to the generator flange 120. The smaller size of the sub-
8 powertrains relative to conventional larger powertrains allows for easy component
9 handling through a nacelle hatch 130.

10
11 **FIGURE 2** is a close-up view of the components of the preferred embodiment
12 shown in **Figure 1**. A seal 200 prevents water leakage, in the case of a current turbine, or
13 fouling, in the case of a wind turbine, of the roller bearings 210 supporting and allowing
14 rotation of the main shaft. The pinions are held in place by bearings 230, 240. Gussets
15 220, 250 in the nacelle structure support the loads transferred from the main shaft to the
16 bearings.

17
18 **FIGURE 3** is an isometric view of the preferred embodiment shown in **Figure 1**.
19 This view more clearly illustrates the interaction between the sun-gear 20 and the pinions
20 30 within the oil-filled chamber 40. The generator, generator flange 110, and gearbox
21 flange 120 are seen to be mounted to the circular plate 100. The pinion bearings 230 are
22 mounted to the walls of the oil-filled chamber 40, which is fortified by structural gussets
23 250.

24
25 **FIGURE 4** shows the side view of a single sub-powertrain in an alternate
26 embodiment of the present invention in which each of the sub-powertrains is mounted on
27 a cylinder 300 that is mounted on the main shaft 310. A torque-dividing gearbox, ring
28 gear 320, is fixed around the inner perimeter of the nacelle. Each of the sub-powertrains
29 is joined via a coupling 370 to a pinion 330. Fluid motion causes the rotors to turn,
30 turning the main shaft and the sub-powertrains mounted to the main shaft. As the sub-
31 powertrain
32

1 spindle rotates, the pinions move past the ring gear within an oil-filled chamber 340,
2 causing the pinions to rotate faster than the main shaft and supplying input power to the
3 sub-powertrains' gearboxes 350. Each gearbox serves to increase the rotational speed of
4 its output shaft relative to its input shaft. The gearbox output shaft is then joined by a
5 coupling 380 to a generator 360. Conduits carrying electricity generated by the sub-
6 powertrains' generators are gathered within the main shaft and transferred to a non-
7 rotating conductor via a slip-ring 390.

8
9 The present invention via a torque-dividing gearbox distributes a high input
10 torque of the rotor 116 between multiple powertrains, each consisting of a smaller
11 conventional torque-reducing gearbox 200 and generator 202. The sum of the power
12 producing capacities of the generators is equal to the maximum power delivered by the
13 power input shaft, and is equivalent to the power produced by a single generator in a
14 conventional system.

15
16 If the spindle consists of a number, n , of smaller powertrains, and the gear ratio
17 between the ring gear and the pinion is m , then the torque, τ' , delivered to each of the
18 gearboxes is given by

$$\tau' = (P/n) / m \omega$$

21 (2)

22
23 where P is the total system input power and ω is the rotational velocity of the spindle. It
24 can be seen that the gearbox input torque, as given in Eq. 1, is reduced by a factor of $(m$
25 $\times n)^{-1}$. In a system consisting of 6 powertrains, with a ring to pinion gear ratio of 15,
26 torque delivered to each gearbox is reduced to 1.11% ($1/90^{\text{th}}$) of the torque of the power
27 input shaft alone.

28
29 **FIGURE 5** is a schematic diagram illustrating prior art (US Patent 4,691,119).
30 This invention couples multiple generators 430 coupled 428 to shafts 426 having pinions
31 425 around a high-speed (low torque) sun gear 420 within the gearbox's second stage.
32 The principal function of this invention is to "create an efficient power supply with a

1 controllable output frequency” to improve the quality of generated electricity for use in
2 avionics. The power input is at high RPM, greatly reducing the need for first stage 410
3 step-up and torque reduction, and therefore reducing the loads applied to the gearbox. A
4 somewhat similar design is used in the invention shown in US Patent 4,585,950, wherein
5 multiple generators are coupled to the high-speed shaft 415 of a wind turbine gearbox for
6 power quality reasons.

7
8 Both of the above prior art designs split the input power at the high-speed end of
9 the gearbox 415, where the input torque applied to each pinion or belt drive is greatly
10 reduced. Instead, the driving shaft upon which the sun gear or belt drive is located could
11 be simply attached to an external gearbox stage or to a single generator. Present
12 understanding of gearbox and generator pricing teaches that high input speed gearboxes
13 are relatively inexpensive, and that multiple generators cost more than a single large
14 generator. In addition, power electronics have been developed to for the functions for
15 which the above inventions have been designed. Therefore, present teaching leads away
16 from use of multiple generators divided at the low-speed shaft of a multi-stage gearbox.

17
18 In comparison, **FIGURE 6** is a schematic diagram of the present invention, which
19 first divides the input torque at the low speed shaft 500 by turning pinions 502 around an
20 input shaft-mounted sun gear 501 before translating it through shafts 504 and couplings
21 506 into multiple independent smaller gearboxes 510, which are then coupled 516 via a
22 shaft 514 to small generators 520. The sun gear 510 and pinions 502 form an effective
23 first stage to the gearbox, while each of the sub-powertrains’ gearboxes 510 are self-
24 contained second stages. The first stage need not be a torque-reducing stage. Instead, it
25 may serve as only a torque-splitter, dividing the load between the separate pinions and
26 distributing the contact load between the teeth on the pinions. The diameter of the sun
27 gear could be the same as the diameter of each pinion, resulting in more of the torque
28 reduction occurring in the individual second stages. The ability to limit the step-up
29 required in the first stage while still resulting in dramatically reduced torque delivered to
30 the second stage results in significant material and associated cost savings.

1 This invention offers a number of solutions not native to conventional powertrains
2 having a single gearbox and generator:

- 3
4 1. The high torque is split between multiple gearboxes, with the input speed to
5 each benefiting from the 5 to 20:1 step up between the ring gear and the
6 pinions. This enables each of the powertrains to consist of commercially
7 available components, with much higher gearbox input speed. This higher
8 input speed and lower power per powertrain results in greatly reduced input
9 torque. The summed cost of these higher speed, lower torque gearboxes is
10 significantly less than the cost of a single low speed, high torque gearbox. In
11 addition, the summed weight of these smaller gearboxes is significantly less
12 than the weight of a single low speed, high torque gearbox.
- 13 2. The parallel powertrains in each nacelle offer an aspect of redundancy that
14 would not be present with a single powertrain, eliminating the single point
15 failure of an individual gearbox and generator. Should one powertrain suffer a
16 fault, it may be taken off line, and the device may continue to generate
17 electricity at a reduced capacity until maintenance is possible.
- 18 3. Efficiency may be boosted by taking powertrains off line when they are not
19 required in lower input power periods. Because generators typically suffer
20 greater efficiency reductions when operating below nominal power input,
21 taking several powertrains off line may allow the remaining powertrains to
22 operate nearer to their optimal efficiency. For instance, if a 750 kW turbine
23 consisted of ten 75 kW systems, then two systems (opposite each other in the
24 ring of powertrains for load balancing) could be taken off line when power
25 production dips below 80%, allowing the remaining generating systems to
26 remain nearer optimal generating efficiency. Typical efficiency gains may be
27 from 1 to 5%, or 20 to 80% reduction in generator losses.
- 28 4. Generator and gearbox cooling may benefit from the reduced mass of
29 individual components and from the spacing of components yielding
30 additional air circulation.

- 1 5. Many of the smaller generating systems available are robustly designed and
2 have very strong performance records, which may help to reduce powertrain
3 faults and expensive maintenance time.
- 4 6. Each powertrain is significantly less massive than a single large powertrain,
5 and may therefore be handled more easily. A significant portion of O&M
6 costs for wind and current turbines come from rental of heavy lifting
7 equipment such as cranes. Because the size of individual components is
8 reduced, the size of the required equipment and the associated costs may be
9 reduced.
- 10 7. Access for maintenance, removal, or replacement is facilitated by the
11 revolving spindle of powertrains. The spindle may be rotated a fraction of a
12 revolution, exposing each powertrain to a single access hatch in the device
13 casing.
- 14 8. The main sun or ring gear and the pinions may be installed to rotate in either
15 direction. This allows for manufacturing and grinding of one set of gearing
16 regardless of the direction of rotation of the main shaft. For some applications
17 it may be advantageous for turbines to rotate in one direction or the other.
18 Because conventional gearboxes are typically designed to rotate in one
19 direction only, two separately designed and manufactured gearboxes would
20 otherwise be required to allow selection of operating direction.
- 21 9. The present invention may be used in conjunction with a fixed pitch, variable
22 speed wind turbine concept. Torque control on the generator may be
23 combined with power electronics to modulate speed. To apply this
24 successfully, a low contact stress gearbox design, such as the present
25 invention, is required in order to handle the associated load excursions.
- 26 10. The present invention may allow maximizing of aerodynamic efficiency in
27 wind turbines. Given the high gear ratios achievable with the present
28 invention in a relatively light and compact configuration, the wind turbine
29 rotor can be operated at lower rotational speeds, which allows for reduction in
30 the blades' tip speed ratio. Operating at a reduced tip speed ratio allows for
31 reduction in blade noise, for reduction in blade surface erosion, and for
32 increases in aerodynamic efficiency due to reduced drag and tip losses.

1
2 While the invention has been particularly shown and described with reference to
3 preferred embodiments thereof, it will be understood by those skilled in the art that the
4 foregoing and other changes in form and detail may be made therein without departing
5 from the scope of the invention.

6
7 All of the numerical and quantitative measurements set forth in this application
8 (including in the claims) are approximations. The invention illustratively disclosed
9 herein suitably may be practiced in the absence of any element which is not specifically
10 disclosed herein.

1 What is Claimed is:

2
1 1. An electric power-generating device comprising:
2 a rotor which revolves in response to an external source of mechanical energy;
3 a main power input shaft coupled to said rotor;
4 a torque-dividing gearbox coupled to said main power input shaft; and,
5 a plurality of torque-reducing gearboxes, each driving a generator and each
6 having an input shaft connected to said torque-dividing gearbox, said plurality of torque-
7 reducing gearboxes being located around a perimeter of said main power input drive
8 shaft.

9
1 2. The electric power-generating device of claim 1 wherein said torque-dividing
2 gearbox includes a stationary ring gear about which said plurality of generators and
3 torque-reducing gearboxes rotate.

4
1 3. The electric power-generating device of claim 1 wherein said torque-dividing
2 gearbox includes a stationary sun gear about which said plurality of generators and
3 torque-reducing gearboxes rotate.

4
1 4. The electric power-generating device of claim 1 wherein said plurality of
2 generators and torque-reducing gearboxes are held stationary with respect to said main
3 power input shaft and said torque-dividing gearbox includes a sun gear which rotates
4 around said perimeter of said main power input shaft.

5
1 5. The electric power-generating device of claim 1 wherein said plurality of
2 generators and torque-reducing gearboxes are held stationary with respect to said main
3 power input shaft and said torque-dividing gearbox includes a ring gear which rotates
4 around said perimeter of said main power input shaft.

5
1 6. The electric power-generating device of claim 1 wherein said torque-dividing
2 gearbox comprises:

3 a ring gear held stationary with respect to said main power input shaft;

4 each input shaft of said plurality of torque-reducing gearboxes being connected
5 through a gearbox to a pinion that engages said ring gear such that as said main power
6 input shaft turns, said generators, torque-reducing gearboxes and pinions rotate around
7 said perimeter of said main power input shaft.

8
1 7. The electric power-generating device of claim 1 wherein said plurality of torque-
2 reducing gearboxes and generators are held stationary with respect to said main power
3 input shaft and said torque-dividing gearbox comprises:

4 a rotating sun gear;
5 each input shaft of said plurality of torque-reducing gearboxes being connected to
6 a pinion that engages said sun gear such that as said main power input shaft turns, said
7 sun gear rotates causing said pinions to turn, driving said torque-reducing gearboxes and
8 said generators.

8. The electric power-generating device of claim 1 wherein said plurality of torque-reducing gearboxes and generators are held stationary with respect to said main power input shaft and said torque-dividing gearbox comprises:

a rotating ring gear;

each input shaft of said plurality of torque-reducing gearboxes being connected to a pinion that engages said ring gear such that as said main power input shaft turns, said ring gear rotates causing said pinions to turn, driving said torque-reducing gearboxes and said generators

9. A device comprising:

a rotor;

a main power input shaft coupled to said rotor;

a torque-dividing gearbox coupled to said main power input shaft; and,

a plurality of torque-reducing gearboxes, each having an input shaft connected to said torque-dividing gearbox, said plurality of torque-reducing gearboxes being located around a perimeter of said main power input shaft.

10. A device comprising:

a rotor;

a main power input shaft coupled to said rotor;

a torque-dividing gearbox coupled to said main power input shaft; and,

a torque-reducing gearbox having an input shaft connected to said torque-dividing gearbox.

11. A device comprising:

a rotor; and

a main power input shaft coupled to said rotor.

12. A device comprising:

a main shaft; and

a gearbox coupled to said shaft.

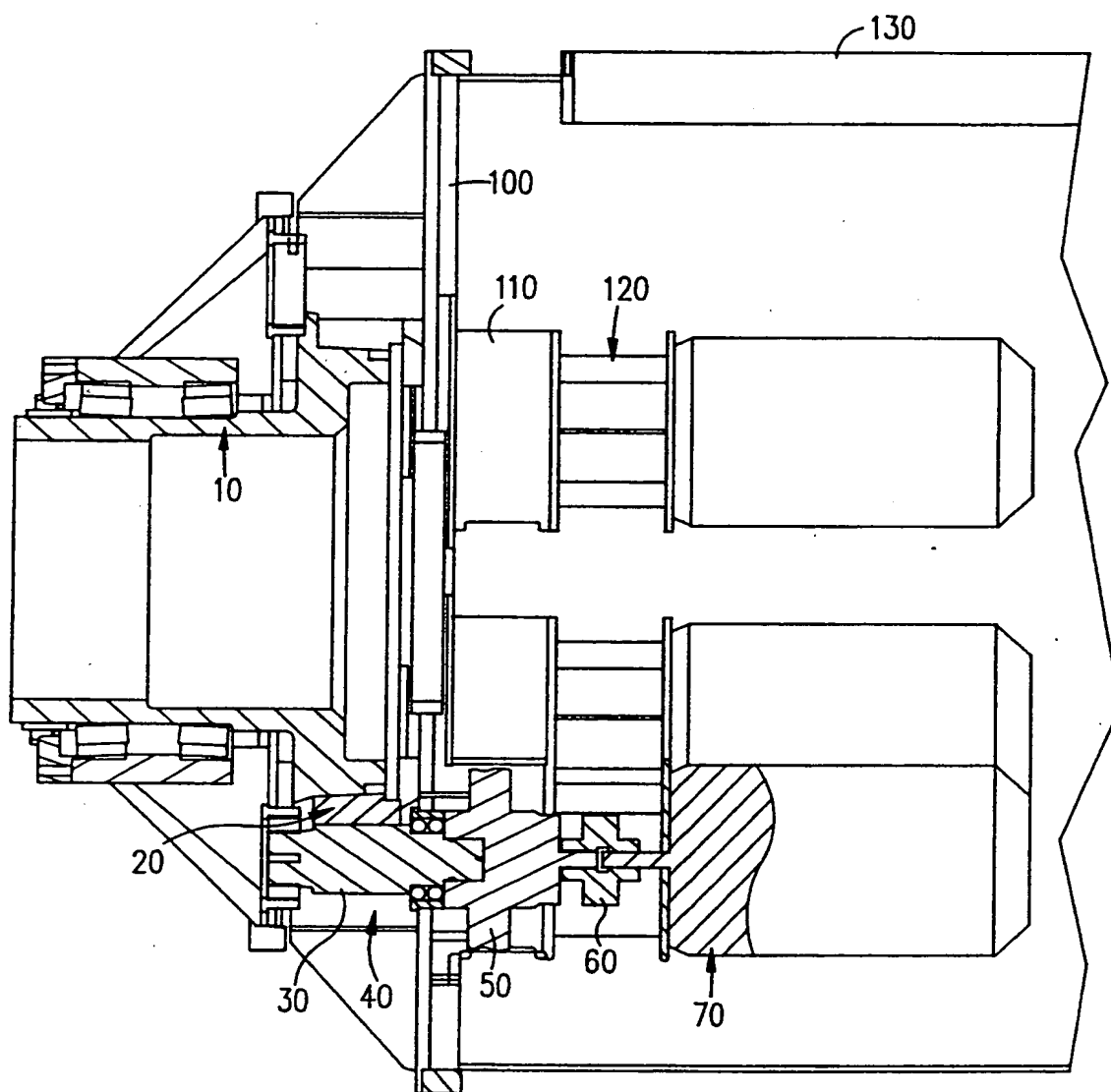


FIG. 1

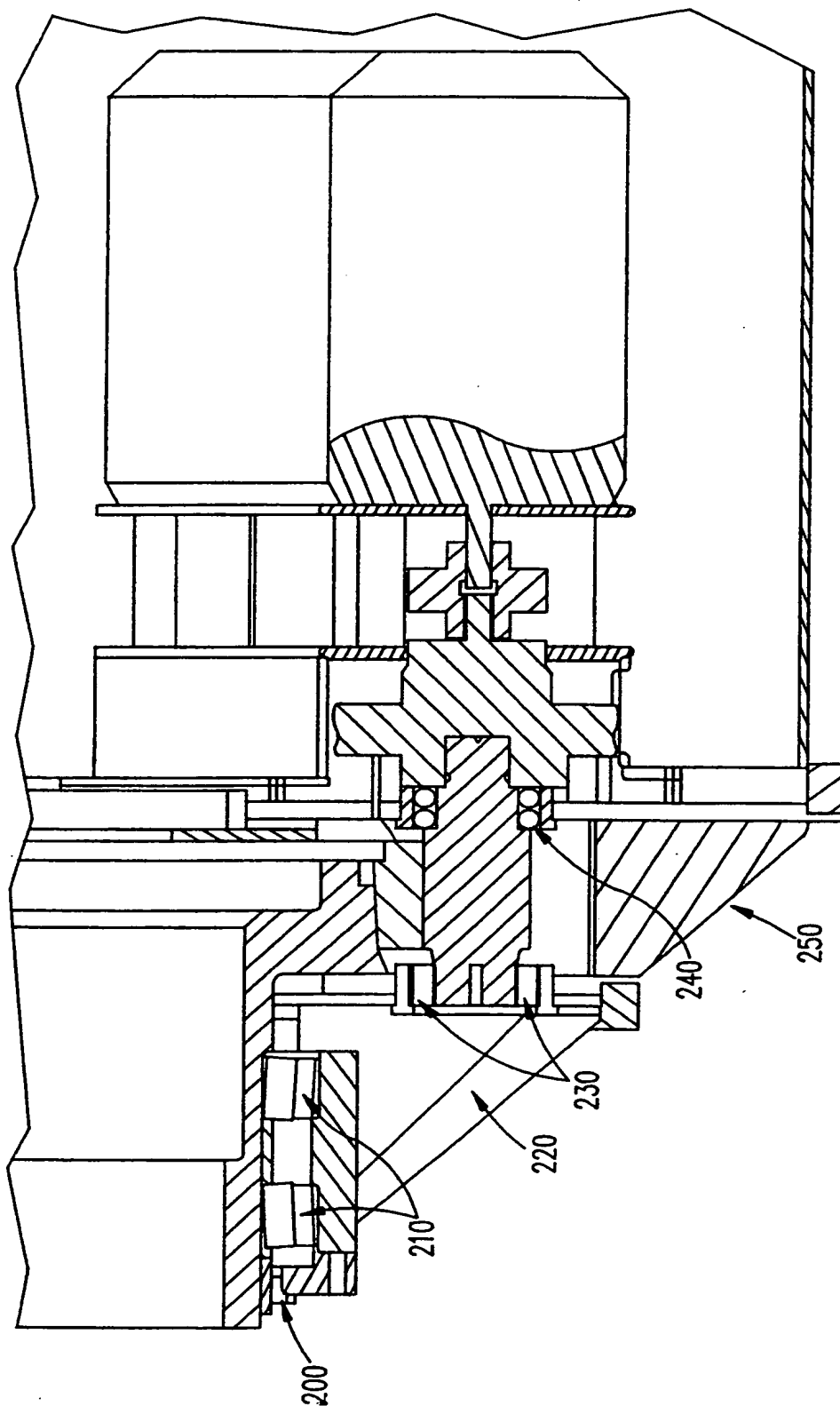


FIG. 2

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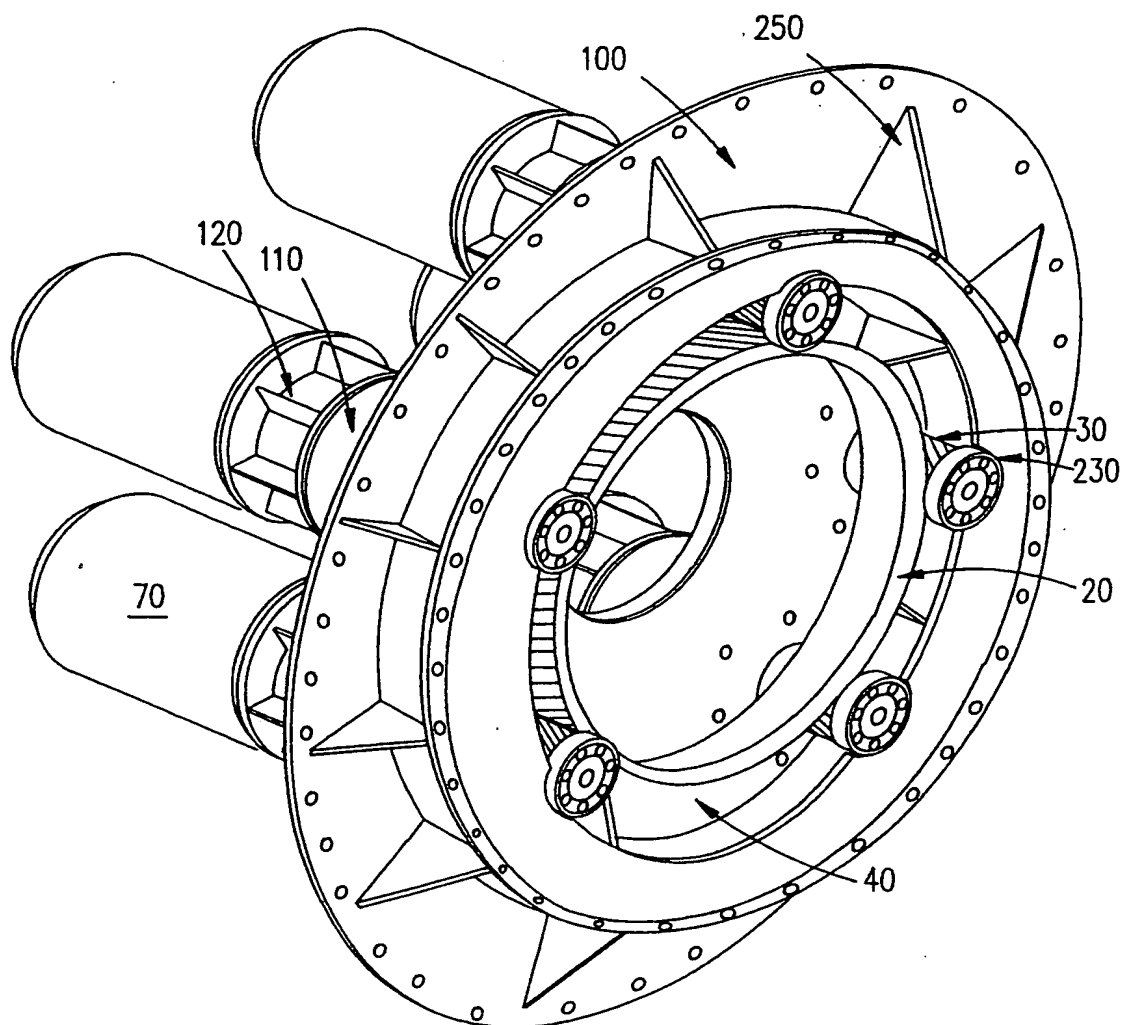


FIG. 3

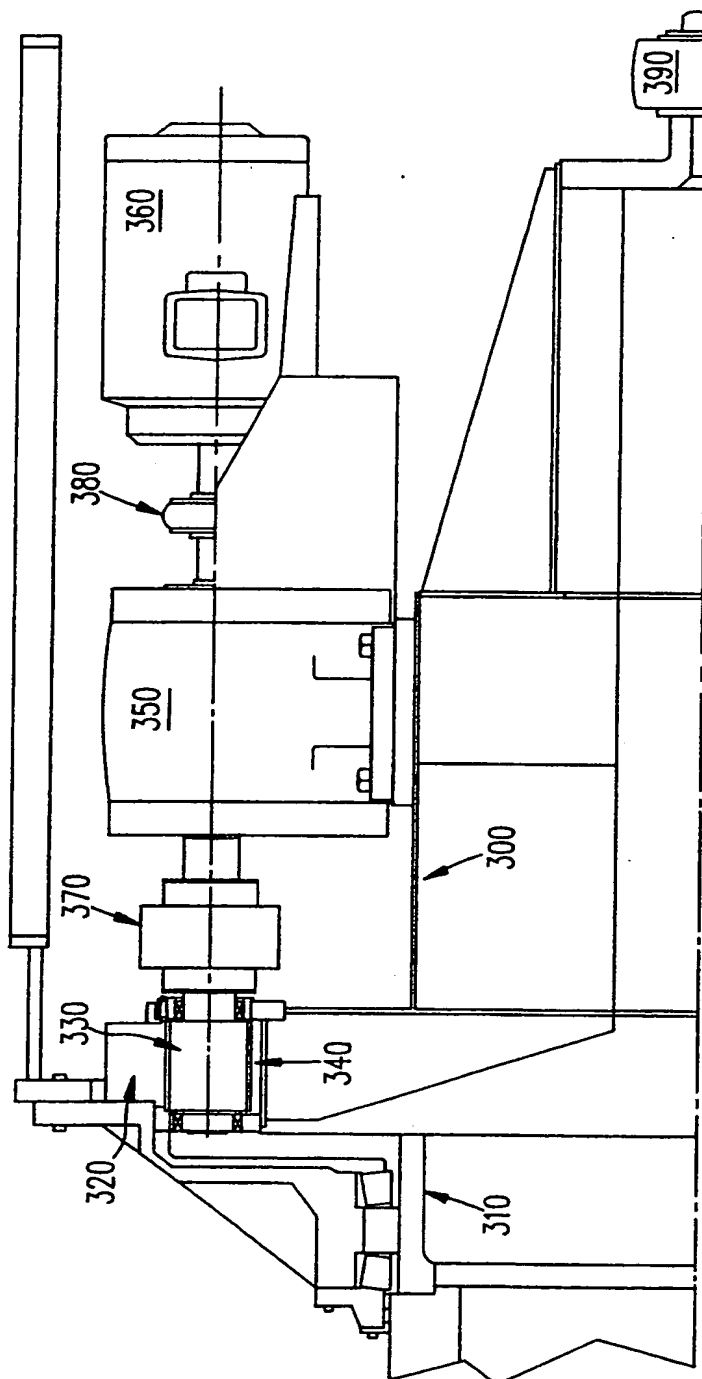


FIG. 4

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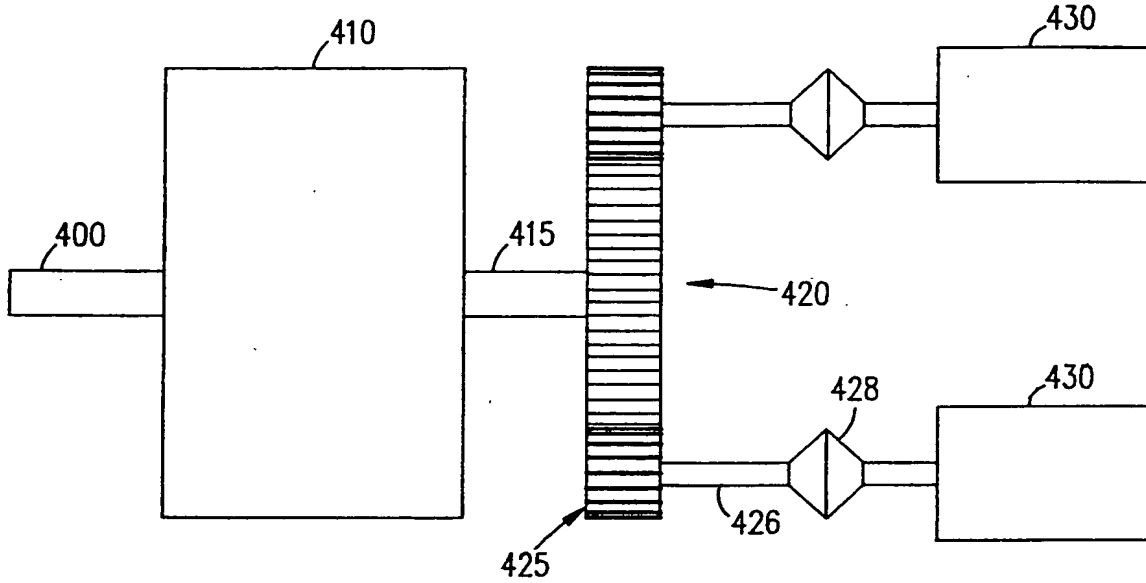


FIG. 5

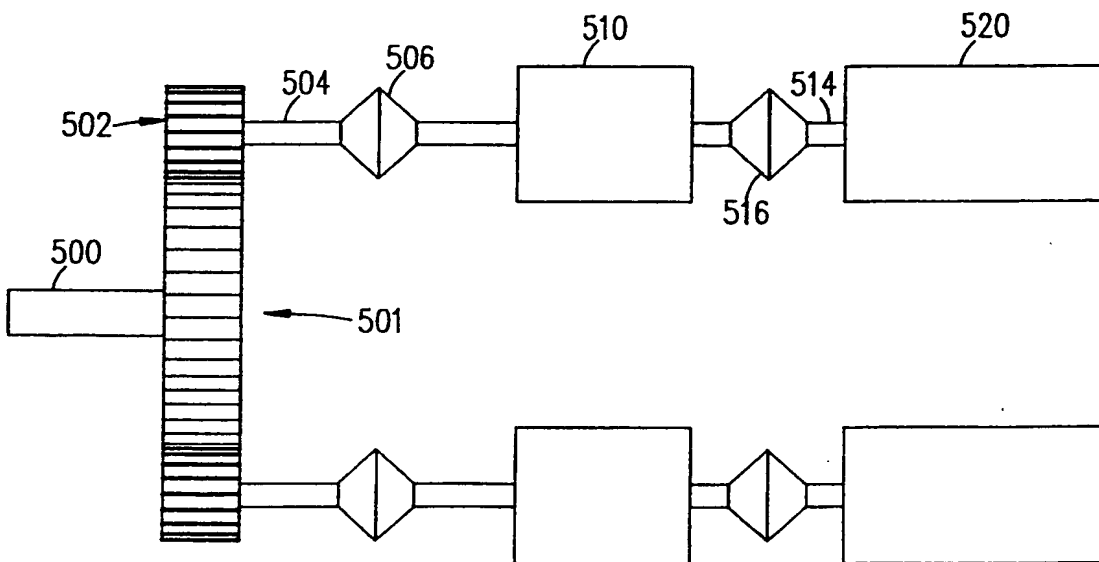


FIG. 6

INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 00/11303

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 H02K16/00 H02K7/116 H02K7/18 F03D11/02

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 H02K F03D

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5 387 818 A (LEIBOWITZ MARTIN N) 7 February 1995 (1995-02-07) column 3, line 62 -column 7, line 63 ---	1-12
X	DE 198 04 177 A (ISUZU CERAMICS RES INST) 10 September 1998 (1998-09-10) column 4, line 43 -column 7, line 65; figures 1-4 ---	1,9-12
A	US 4 848 188 A (SCHUMACHER LARRY L) 18 July 1989 (1989-07-18) column 3, line 1 -column 4, line 68; figures 1,2 ---	1-12
A	US 4 691 119 A (MCCABRIA JACK L) 1 September 1987 (1987-09-01) cited in the application -----	

☐ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

* Special categories of cited documents :

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Date of the actual completion of the international search

6 September 2000

Date of mailing of the international search report

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Name and mailing address of the ISA

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NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,
Fax: (+31-70) 340-3016

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INTERNATIONAL SEARCH REPORT

Information on patent family members

Inter. Patent Application No

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